

Unity feedback system.  
 $H(s) = 1$

Then

$$e_{ss} = \lim_{s \rightarrow 0} s \frac{R(s)}{1 + G(s)}$$

Then, from above equation it is clear that the steady state error depends upon input and closed loop transfer function.

### STATIC ERROR COEFFICIENTS

Static position error constant (or coefficient)  $k_p$ .

$\therefore$  we know that:

$$e_{ss} = \lim_{s \rightarrow 0} s \cdot \frac{R(s)}{1 + G(s) \cdot H(s)}$$

For unit step input

$$R(s) = \frac{1}{s}$$

$$e_{ss} = \lim_{s \rightarrow 0} s \cdot \frac{1}{s(1 + G(s) \cdot H(s))}$$

$$e_{ss} = \frac{1}{1 + \lim_{s \rightarrow 0} G(s) \cdot H(s)}$$

put  $k_p = \lim_{s \rightarrow 0} G(s) \cdot H(s)$  is called static position error constant.

$$\therefore e_{ss} = \frac{1}{1 + k_p}$$

$$e_{ss} = \frac{1}{1 + k_p}$$

and

$$k_p = \lim_{s \rightarrow 0} G(s) \cdot H(s)$$

Q15 State velocity constant  $k_v$  (or coefficient)  $k_v$

∴ we know that

The static steady state error is given by:

$$e_{ss} = \lim_{s \rightarrow 0} s \cdot \frac{R(s)}{1 + G(s)H(s)}$$

For unit ramp input

$$R(s) = \frac{1}{s^2}$$

put in above equation we get:

$$e_{ss} = \lim_{s \rightarrow 0} s \cdot \frac{1}{s^2 [1 + G(s)H(s)]}$$

$$= \lim_{s \rightarrow 0} \frac{1}{s [1 + G(s)H(s)]}$$

$$= \lim_{s \rightarrow 0} \frac{1}{s + sG(s)H(s)} = \lim_{s \rightarrow 0} \frac{1}{0 + sG(s)H(s)}$$

$$= \lim_{s \rightarrow 0} \frac{1}{G(s)H(s) \cdot s}$$

$$= \frac{1}{k_v}$$

where

$$k_v = \lim_{s \rightarrow 0} s \cdot G(s)H(s)$$

hence

$$k_v = \lim_{s \rightarrow 0} s G(s)H(s)$$

is called static velocity constant.

and

$$e_{ss} = \frac{1}{k_v}$$

State acceleration error constant (Coefficient)  $K_a$ .  
 The steady state error with unit parabolic input is given by:

$$e_{ss} = \lim_{s \rightarrow 0} s \cdot \frac{R(s)}{1 + G(s) \cdot H(s)}$$

For unit parabolic input  
 $R(s) = \frac{1}{s^2}$

$$e_{ss} = \lim_{s \rightarrow 0} s \cdot \frac{1}{s^2 [1 + G(s) \cdot H(s)]}$$

$$= \lim_{s \rightarrow 0} \frac{1}{s [1 + G(s) \cdot H(s)]}$$

$$= \frac{1}{0 + [\lim_{s \rightarrow 0} s^2 G(s) \cdot H(s)]}$$

put  $\lim_{s \rightarrow 0} s^2 G(s) \cdot H(s) = K_a$

$$e_{ss} = \frac{1}{K_a}$$

State acceleration constant

$$K_a = \lim_{s \rightarrow 0} s^2 G(s) \cdot H(s)$$

## CLASSIFICATION OF CONTROL SYSTEM

Consider the open loop transfer function

$$G(s)H(s) = \frac{K(1+sT_z)(1+sT_b) \dots}{s^m(1+sT_a)(1+sT_b) + \dots} \quad \text{--- (1)}$$

The poles of the system are at  $s = -\frac{1}{T_a}, -\frac{1}{T_b}$  and  
 zeros at  $s = -\frac{1}{T_z}, \frac{1}{T_b}$

The term 'pm' gives the number of poles at origin.

**Type '0' system:** A system having no pole at origin of the 's' plane is said type '0' system. i.e.  $m=0$

**Type '1' system:** If a system having a single pole at origin of 's' plane is said to be type '1' system.

For type-1 system  $s \geq 1$ .

**Type '2' systems:** If a system having two poles at origin of the s-plane is called type-2 system.

For type-2 system,  $m=2$ .

1) **Type '0' system with unit step input:**

∴ Open loop transfer function is given by

$$G(s)H(s) = \frac{k(1+sT_1)(1+sT_2)}{(1+sT_a)(1+sT_b)}$$

$$k_p = \lim_{s \rightarrow 0} G(s)H(s)$$

$$\lim_{s \rightarrow 0} \frac{k(1+sT_1)(1+sT_2)}{(1+sT_a)(1+sT_b)} = k$$

$$e_{ss} = \frac{1}{1+k_p} = \frac{1}{1+k}$$

$$e_{ss} = \frac{1}{1+k}$$

2) **Type '0' system with unit ramp input:**

Q.P. As we know that:

$$K_v = \lim_{s \rightarrow 0} s G(s) H(s)$$

$$= \lim_{s \rightarrow 0} s \cdot \frac{k(1+sT_1)(1+sT_2)}{(1+sT_a)(1+sT_b)} = 0$$

$$\text{ess} = \frac{1}{K_v} = \frac{1}{0} = \infty$$

Type '0' system with unit parabolic input:

$$Q.P. K_a = \lim_{s \rightarrow 0} s^2 G(s) H(s)$$

$$= \lim_{s \rightarrow 0} s^2 \frac{k(1+sT_1)(1+sT_2)}{(1+sT_a)(1+sT_b)}$$

$$= 0$$

$$\text{ess} = \frac{1}{K_a} = \frac{1}{0} = \infty$$

Type '1' system with (unit)

Type '1' system with unit step input

Q.P. We know that:

$$G(s)H(s) = \frac{k(1+sT_1)(1+sT_2)}{(1+sT_a)(1+sT_b)}$$

$$K_p = \lim_{s \rightarrow 0} G(s) \cdot H(s)$$

$$= \lim_{s \rightarrow 0} \frac{k(1+sT_1)(1+sT_2)}{s(1+sT_a)(1+sT_b)}$$

$$= \infty$$

$$\text{ess} = \frac{1}{1+K_p} = \frac{1}{1+\infty} = 0$$

2) Type-1 system with unit ramp input:

$$K_v = \lim_{s \rightarrow 0} s G(s) H(s)$$

$$= \lim_{s \rightarrow 0} \frac{k(1+sT_1)(1+sT_2) \dots}{s(1+sT_0)(1+sT_b)}$$

$k$

$$e_{ss} = \frac{1}{K_v} = \frac{1}{k}$$

3) Type-1 system with unit parabolic input:

$$K_a = \lim_{s \rightarrow 0} s^2 G(s) H(s)$$

$$= \lim_{s \rightarrow 0} \frac{k(1+sT_1)(1+sT_2) \dots}{s^2(1+sT_0)(1+sT_b)}$$

$$= \lim_{s \rightarrow 0} \frac{s k (1+sT_1)(1+sT_2) \dots}{(1+sT_0)(1+sT_b)}$$

0

$$e_{ss} = \frac{1}{K_a} = \frac{1}{0} = \infty$$

Type '2' system

1) With unit step input:

we know that for type-2 system

$$G(s) H(s) = \frac{k(1+sT_1)(1+sT_2) \dots}{s^2(1+sT_0)(1+sT_b)}$$

$$K_p = \lim_{s \rightarrow 0} G(s) H(s) = \infty$$

$$e_{ss} = \frac{1}{K_p} = \frac{1}{\infty} = 0$$

with unit ramp input:

$$e_{ss} \approx K_v = \lim_{s \rightarrow 0} s G(s) H(s)$$

$$= \lim_{s \rightarrow 0} \frac{s \cdot K (1+sT_1)(1+sT_2) \dots}{s^2 (1+sT_a)(1+sT_b) \dots}$$

$$= \lim_{s \rightarrow 0} \frac{1}{s} \cdot \frac{K (1+sT_1)(1+sT_2) \dots}{(1+sT_a)(1+sT_b) \dots}$$

$\infty$

$$e_{ss} = \frac{1}{K_v} = \frac{1}{\infty} = 0$$

parabolic

with unit ramp input

$$e_{ss} \approx K_a = \lim_{s \rightarrow 0} s^2 G(s) H(s)$$

$$= \lim_{s \rightarrow 0} \frac{s^2 \cdot K (1+sT_1)(1+sT_2) \dots}{s^3 (1+sT_a)(1+sT_b) \dots}$$

$\infty$

$$e_{ss} = \frac{1}{K_a} = \frac{1}{\infty}$$

	Type '0' system	Type '1' system	Type '2'
Unit step input	$\frac{1}{1+K}$	0	0
Unit ramp input	$\infty$	$\frac{1}{K}$	0
Unit parabolic input	$\infty$	$\infty$	$\frac{1}{K}$